



Article

A Novel Algorithm for Recovering Out-of-Service Loads in Smart Distribution Systems Following Exposure to Cyber-Attacks

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Abstract

An algorithm is proposed to recover out-of-service loads (OOSLs) in smart distribution systems (SDSs) after exposure to cyber-attacks (CAs) resulting in interruptions of in-service loads (INSLs). The proposed algorithm is implemented in three steps. The first step is based on building the SDS in matrix form to be data input to the proposed algorithm. The second step is concerned with classifying the SDS into three zones: the attacked zone, the primary neighbor zone, and the secondary neighbor zone. The third step is performing five maneuvering processes (MPs) to recover the OOSL without breaking the electric limitations (ELs). The ELs are related to the maximum branch current, the node voltage, the load priority, the radiality maintenance of the SDS, the minimum system total power loss, the instruction sequence of the automatic-communication-switches (ACS), and the minimum number of ACSs. The proposed algorithm was tested under a 70-bus SDS with four electric supply feeders. The proposed algorithm achieved supply recovery for all OOSLs with efficiency of 100% after the occurrence of a CA on a single or double ACS without breaking the ELs. The proposed algorithm succeeded in achieving supply recovery for 97.6%, 97.1%, and 96.4% of the OOSLs after the simultaneous occurrence of a CA on three, four, and five ACSs, respectively, without breaking the ELs. The advantages of the proposed algorithm are a lack of dependency on the system size, a short electric supply recovery time within the range of 190-199 ms, a lack of dependency on distributed generation (DG), and the achievement of self-healing in the SDS following a single and two simultaneous CAs, as well as almost achieving self-healing under exposure to three, four, and five simultaneous CAs.

Keywords: cyber-attack; smart distribution system; out-of-service loads; electric service recovery; zone classification; self-healing; maneuvering processes



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1. Introduction

An SDS contains a high level of software that enables electrical components to be highly controllable, secure, and self-healing [1]. This software communicates with the control system, protection system, information technology components, operational technology components, advanced metering infrastructure, supervisory control and data acquisition (SCADA) components, measurement devices, distributed generation, and main electrical components. As the distribution system contains a lot of software, the probability of being exposed to hacking is high. CAs are one of the most important challenges that modern smart distribution systems face [2].

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There are three directions in research related to CAs in SDSs. The first direction is concerned with how CAs affect SDSs. CAs can affect electrical components and protocol devices. The electrical components include generators, electric vehicles, transmission lines, transformers, and automatic controlled switches [3–7]. The protocol components include advanced metering systems, server infrastructure, routers, SCADA systems, wireless communication signals, and Internet of Things (IoT) technologies. Cyber-attacks in such systems often involve injecting false data to generate incorrect commands [8–11].

The second direction of research discusses the impact of CAs on SDSs, which can lead to the complete or partial shutdown of electricity distribution. Smart distribution systems are designed to optimize power delivery. A CA could disable optimization algorithms, leading to inefficient load balancing and overloading certain parts of the grid, while others remain partly loaded, with potential to cause local failures. Attackers could gain remote access to an SDS to manipulate equipment settings, disable monitoring, or make unauthorized changes. This could result in malfunctioning, the destruction of equipment, or the theft of data [12–15].

The third direction discusses how to block a chain of CAs in an SDS. Advanced firewalls are used to monitor and filter network traffic, protecting the grid from unauthorized access and potential threats. Systems are set up to detect and stop harmful or suspicious activity on a network. Segmenting the network into smaller, isolated parts can prevent the harm from spreading. For example, separating operational technology (OT) networks from information technology (IT) networks can localize the attacked area. Strong encryption is used to protect data transition between smart meters, substations, control centers, and other devices. This ensures that sensitive data cannot be intercepted or altered by attackers. The regular back-up of system configurations, critical data, and software is performed [16–20].

The current paper presents, for the first time, a new research direction toward the supply recovery of the OOSL following a CA hitting an SDS. To the authors' knowledge, this may be the first work that addresses the supply recovery of the OOSL of an SDS exposed to a CA hitting the ACS, because the related research in the literature is limited.

In 2015, the power distribution network of Western Ukraine was cyber-attacked, causing 225 thousand households to be out of service for two hours [21]. In 2016, the power distribution network of Kyiv was attacked by hackers, leaving end-users without ES for six hours [22]. In 2014, a CA hacked South Korean power generation networks to interrupt the ES of 50 thousand end-users for 3 h [23]. In 2017, a CA was directed against Saudi Arabian power transmission systems, causing a supply interruption for 12 h [24]. In 2003, a blackout occurred in the United States and Canada due to large CAs causing a delusional fault in the utility systems, so the protection systems took incorrect actions [25].

The occurrence of CAs in SDSs hinders the self-healing of SDSs. The supply recovery of the OOSL following a CA is the responsibility of the recovery algorithm [26]. The difference between a fault and a CA imposed on an SDS is that a fault causes a faulty load and OOSL but the CA leaves only the OOSL [26]. Figure 1 shows a 15-bus SDS with three electric supply feeders. A CA hits the SDS at ACS No. 1, causing the downstream loads from A through D to be OOSLs; see Figure 2. The objective of the proposed algorithm is to restore the ES for the OOSL without breaking the EL.

The proposed algorithm ultimately prevents hackers from achieving their goal to turn off the electrical distribution systems. The proposed algorithm adds to the software of the smart grid in rendering it more automated, secure, and self-healing. The proposed algorithm increases the resilience of distribution networks in exposure to cyber-wars, such as the one that occurred in 2025 when Pakistani hackers launched a CA to target Indian power systems. The proposed algorithm can be implemented in the control centers or

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intelligent electronic devices of the smart distribution system or in the resilience modules in the energy management system.

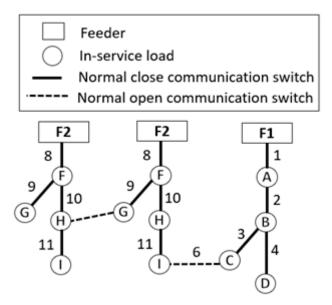


Figure 1. A 15-bus SDS with three feeders, F1 through F3, in a rectangular shape; the solid line represents the normally closed ACS, the dashed line indicates the normally open ACS, and the circle represents the INSL.

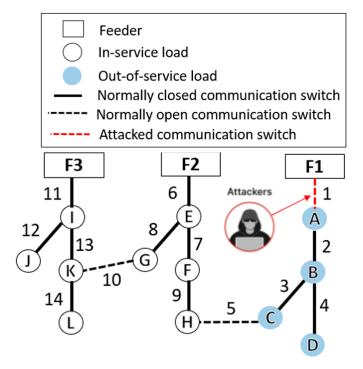


Figure 2. Cyber-attack at ACS No. 1, which connects node F1 with node A, in a 15-bus SDS with three feeders, F1 through F3, represented in a rectangular shape. The solid black line represents the normally closed ACS, the dashed black line indicates the normally open ACS, the white circle represents the INSL, the blue circle indicates the OOSL, and the dashed red line represents an attacked ACS.

The reliability and resilience of a 39-bus and IEEE 30-bus system was enhanced by 22% [27] after experiencing a CA by enabling the system to recover from the threat. The number of maintenance personnel was increased after the occurrence of a CA to recover the ES for the OOSL [28]. The ability of the SDS to withstand a CA was enhanced by using

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a large number of electric vehicles as distributed generators to feed the OOSL after the occurrence of a CA [29]. A part of the outage area was restored after experiencing a CA by adding DG resources to support the smart distribution system against CAs [30]. An optimized algorithm based on mixed-integer linear programming was proposed to handle load interruptions following a CA. This algorithm was based on the philosophy of first fail first repair [31].

The originality and novelty of this paper are represented as follows:

- (i). A novel algorithm is proposed for the first time to recover the ES for the OOSL after the occurrence of a CA on an ACS in the SDS, regardless of whether the CA occurs on a single or multiple ACSs.
- (ii). The proposed algorithm takes into consideration the EL regarding (a) the maximum feeder current, (b) the voltage limits of each node, (c) the load priority, (d) the radiality maintenance of the SDS, and (d) the instruction sequence of the ACS, as well as minimizing their number and (f) achieving the minimum total system power loss.
- (iii). The proposed algorithm shows better performance irrespective of the (a) number of OOSLs, (b) system size, (c) operation with or without DGs, and (d) number of simultaneous CAs.
- (iv). The proposed algorithm shows better performance according to (a) the time of electric service recovery, (b) the ability to achieve self-healing, and (c) testing under single and simultaneous CAs.

The rest of the paper is organized as follows. Section 2 addressees the proposed algorithm. Section 3 contains the results obtained on applying the proposed algorithm to a 70-bus SDS with four electric supply feeders exposed to CAs. Section 4 contains the conclusions.

2. Proposed Algorithm

The novelty and originality of the proposed algorithm is based on achieving the self-healing goal after the occurrence of a single or simultaneous CAs hitting the ACS in the SDS, without breaking seven ELs. In this context, the goal of the proposed recovery algorithm is to guarantee the continuity of the ES to the OOSL following exposure to a CA as early as possible, without breaking the ELs, which are as follows.

Electric limitation 1 (EL1): This limitation is concerned with the maximum branch current and node voltage limits. It is forbidden to transfer loads in the maneuvering process to a branch if it becomes overloaded or the voltage limit is exceeded. The overloading causes an outage for all loads connected to the overloaded branch, without recovering the OOSL.

Electric limitation 2 (EL2): The proposed algorithm should guarantee that the system is radial after the maneuvering process (MP).

Electric limitation 3 (EL3): The proposed algorithm should take into consideration the load priority. For this reason, the recovery algorithm should first recover the OOSL with the highest priority index before those with lower priority.

Electric limitation 4 (EL4): The proposed algorithm should minimize the total system power loss by performing system reconfiguration.

Electric limitation 5 (EL5): The proposed algorithm should minimize the number of commanded ACSs when recovering the OOSL.

Electric limitation 6 (EL6): The proposed algorithm should take into consideration the sequence of the commanded ACSs.

Electric limitation 7 (EL7): The proposed algorithm should restore the OOSL upon the occurrence of simultaneous CAs. Multiple cyber-attacks can simultaneously target the same number of automatic communication switches. This means that each cyber-

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attack is responsible for changing the state of a single switch from closed to open, thereby disconnecting all downstream loads from the power supply. In other words, each CA hits only one automatic switch.

The proposed algorithm is based on three sequential steps as follows.

Step 1: This step is responsible for defining the data of the SDS to serve the proposed algorithm, regardless of the system size of the SDS, with/without DGs. This points to two advantages of the proposed algorithm: (a) independence from the system size and (b) independence from the DGs. It is worth mentioning that the proposed algorithm is independent of the complexity of the CAs because the implementation of the proposed algorithm occurs after the CA. The data should be defined for the proposed algorithm in matrix form, as shown in Figure 3. This matrix consists of three rows, and the number of columns is equal to the number of ACSs in the SDS. Each column consists of the switch connecting the upstream node and the downstream node. The switch is defined by its name and its status, e.g., C represents a closed status and O represents an open status. Figure 3 provides a representation of the 15-bus SDS that is shown in Figure 1 in matrix form, serving as data input for the proposed algorithm. For example, the first column represents a normally closed switch, No. 1, linking upstream node F1 to downstream node A. The second column represents a normally closed switch, No. 2, linking upstream node A to downstream node B.

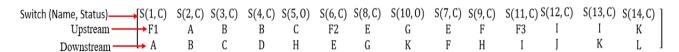
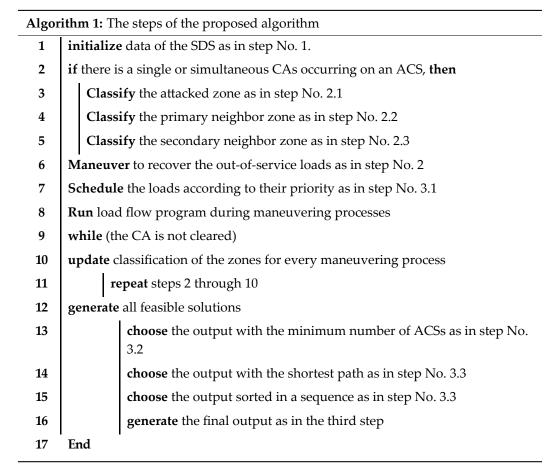


Figure 3. Illustration of data definition of SDS for proposed algorithm.

- **Step 2**: This step is responsible for dividing the SDS into three zones after the occurrence of a CA as follows.
- **Step 2.1:** "The attacked zone" includes the OOSL zone, which includes all downstream OOSLs, as sown in Figure 4.
- **Step 2.2**: "The primary neighbor zone" accommodates loads that link directly to the attacked zone only through a normally open ACS, as shown in Figure 4. This normally open ACS is responsible for performing the first maneuvering process for automatic load transfer from the attacked zone to the primary neighbor zone.
- **Step 2.3**: "The secondary neighbor zone" accommodates the loads that link the secondary neighbor zone through a normally open ACS (Figure 4) to perform the second maneuvering process, which is represented by redistributing the loads among the primary and secondary neighbor zones after breaking the EL related to the maximum feeder current in the first maneuvering process.
- **Step 3:** This step is responsible for generating one feasible solution among several ones as follows.
- **Step 3.1:** If there is more than one maneuvering process, the proposed algorithm performs the maneuvering process that feeds the highest-priority loads.
 - **Step 3.2:** The proposed algorithm arranges the ACS to feed the largest load first.
- **Step 3.3:** If the proposed algorithm generates more than one feasible solution, the algorithm chooses the solution that achieves the following:
- (i). The minimum number of ACSs;
- (ii). The minimum power loss as estimated by a load flow study.The steps of the proposed algorithm are described in Algorithm 1.

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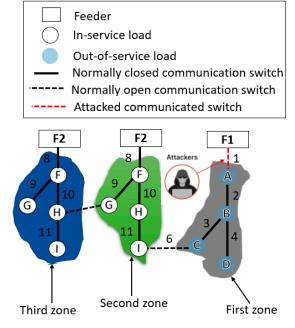


Figure 4. Division of the smart distribution system into three zones after the occurrence of a CA; the black zone represents the attacked zone, the green zone indicates the primary neighbor zone, and the blue zone represents the secondary neighbor zone.

3. Results and Discussion

The proposed algorithm is based on achieving self-healing after the occurrence of a single or simultaneous CAs hitting the ACS in the SDS, without breaking seven ELs. Figure 5 shows the SDS used for the testing of the proposed algorithm. This system consists

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of a 70-bus setup with four electric supply feeders. In power engineering terminology, tie and sectionalize switches are adopted. However, the terminology used here refers to these switches as normally open communication and normally closed communication switches, respectively. The circle represents the load, the solid line represents a normally closed ACS, and the dashed line represents a normally open ACS, while the rectangle represents the feeder. There is a priority index assigned to each load, i.e., high, medium, and low. It is worth mentioning that the efficiency of the proposed algorithm following the occurrence of a CA does not change according to the priority index of the load.

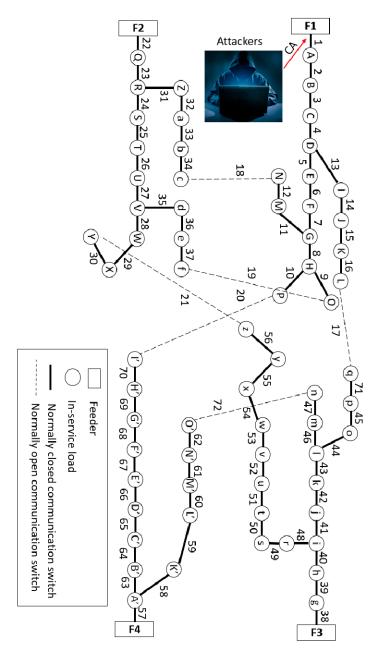


Figure 5. A 70-bus power distribution system with four electric supply feeders, F1 through F3, indicated with rectangles; the white circle represents the INSL, the solid line indicates a normally closed ACS, and the dashed line represents a normally open ACS.

The performance of the proposed algorithm is evaluated as follows:

1. The recovery efficiency is equal to the ratio of the number of successful cases to the number of all possible cases.

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- 2. The recovery time represents the time from the occurrence of the CA until the time of recovery of the OOSLs.
- 3. The following seven electric limitations (ELs) are satisfied:
 - 3.1 EL1 addresses the maximum branch current and node voltage limits.
 - 3.2 EL2 guarantees the maintenance of system radiality.
 - 3.3 EL3 considers the load priority.
 - 3.4 EL4 aims at minimizing the total system power loss.
 - 3.5 EL5 aims at minimizing the number of commanded ACSs.
 - 3.6 EL6 considers the sequence of the commanded ACSs.
 - 3.7 EL7 restores OOSLs with the occurrence of simultaneous CAs.

3.1. Electric Service Recovery in SDS Following Exposure to Single CA

The number of possible cases of a single CA is equal to 66. Table 1 shows the performance of the proposed algorithm under all possible cases of a single CA. The proposed algorithm achieves supply recovery for all OOSLs with efficiency of 100% after the occurrence of a CA on a single ACS, without breaking the ELs. For example, consider a single CA occurring at ACS No. 1, which results in disconnecting load nodes from A through P. The proposed algorithm generates feasible outputs in the sequence SW_{13}^O , SW_8^O , SW_{18}^C , SW_{17}^C , SW_{20}^C , which results in supply recovery for all OOSLs in 194 ms without breaking the ELs.

Table 1. Performance of the proposed algorithm under all possible maneuvering processes following a single CA hitting the investigated 70-bus test system with four electric supply feeders.

Location of Attacked Switch	OOSL	Output of Proposed Algorithm	T _{est} (ms)	RL	EL ₁	EL ₂	EL ₃	EL ₄	EL ₅	EL ₆	EL ₇
1	A-P	$SW_{13}^{O} \\ SW_{8}^{O} \\ SW_{18}^{C} \\ SW_{17}^{C} \\ SW_{20}^{C}$	194	A-P	√	✓	✓	✓	✓	✓	✓
2	B-P	SW ₅ ^O SW ₁₇ ^C SW ₁₉ ^C	190	В-Р	√	√	√	√	√	√	✓
3	С-Р	SW ₆ ^O SW ₁₇ ^C SW ₁₈ ^C	191	С-Р	√	✓	✓	✓	✓	✓	✓
4	D-P	SW ₅ ^O SW ₁₇ ^C SW ₁₉ ^C	191	D-P	√	✓	✓	✓	√	✓	√
5	E-H, O-P, N-M	SW ^C ₁₈	193	E-H, O-P, N-M	✓	✓	✓	✓	✓	✓	✓
6	F-H, O-P, N-M	SW ^C ₁₉	197	F-H, O-P, N-M	✓	✓	✓	✓	✓	✓	✓
7	G-H, O-P, N-M	SW ₂₀ ^C	196	G-H, O-P, N-M	✓	✓	✓	✓	✓	✓	✓
8	Н, О-Р	SW_{20}^C	196	Н, О-Р	✓	✓	✓	✓	✓	✓	✓
9	О	SW ₁₉ ^C	197	О	✓	✓	✓	✓	✓	✓	✓
10	P	SW ₂₀ ^C	190	P	✓	✓	✓	✓	✓	✓	✓
11	M-N	SW ₁₈ ^C	190	M-N	✓	✓	✓	✓	✓	✓	✓
12	N	SW ₁₈ ^C	197	N	✓	✓	✓	✓	✓	✓	✓

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 Table 1. Cont.

Location of Attacked Switch	OOSL	Output of Proposed Algorithm	T _{est} (ms)	RL	EL ₁	EL ₂	EL ₃	EL_4	EL ₅	EL_6	EL ₇
13	I-L	SW ^C ₁₇	198	I-L	✓	√	√	√	√	√	✓
14	J-L	SW ^C ₁₇	195	J-L	✓	✓	✓	✓	✓	✓	√
15	K-L	SW ^C ₁₇	195	K-L	√	✓	✓	✓	✓	✓	√
16	L	SW ^C ₁₇	196	L	√	√	✓	√	√	√	√
22	Q-Z, a-f	SW ₂₅ SW ₂₈ SW ₁₈ SW ₁₉ SW ₂₁	196	Q-Z, a-f	√	√	√	√	√	√	✓
23	R-Z, a-f	SW ₂₅ SW ₀ O SW ₂₈ SW ₁₈ SW ₁₉ SW ₂₁ C	197	R-Z, a-f	✓	✓	✓	✓	✓	✓	✓
24	S-Y, d-f	SW ^O ₂₈ SW ^C ₁₉ SW ^C ₂₁	196	S-Y, d-f	✓	√	√	✓	✓	√	√
25	T-Y, d-f	$SW_{28}^{O} \ SW_{19}^{C} \ SW_{21}^{C}$	194	T-Y, d-f	✓	✓	✓	√	✓	√	✓
26	U-Y, d-f	SW_{19}^C	190	U-Y, d-f	✓	✓	✓	✓	✓	✓	✓
27	V-Y, d-f	SW_{19}^C	191	V-Y, d-f	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	✓
28	W-Y	SW_{21}^{C}	193	W-Y	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	✓
29	X-Y	SW_{21}^{C}	197	X-Y	✓	✓	✓	✓	✓	✓	✓
30	Y	SW_{21}^{C}	196	Y	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	✓
31	Z, a-c	SW_{18}^C	195	Z, a-c	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	✓
32	a-c	SW_{18}^{C}	196	а-с	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	✓
33	b-c	SW_{18}^C	197	b-c	\checkmark	✓	✓	✓	\checkmark	\checkmark	✓
34	C	SW_{18}^C	190	С	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	✓
35	d-f	SW_{19}^C	194	d-f	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	✓
36	e-f	SW_{19}^C	190	e-f	\checkmark	\checkmark	✓	\checkmark	\checkmark	\checkmark	✓
37	F	SW ^C ₁₉	191	F	✓	✓	✓	✓	✓	✓	✓
38	g-z	SW ^O ₄₁ SW ^C ₁₇ SW ^C ₂₁	195	g-z	✓	✓	✓	√	√	√	✓
39	h-z	SW ^O ₄₁ SW ^C ₁₇ SW ^C ₂₁	197	h-z	✓	✓	✓	✓	✓	✓	✓
40	i-z	SW ^O ₄₁ SW ^C ₁₇ SW ^C ₂₁	190	i-z	✓	✓	✓	√	√	√	✓

Table 1. Cont.

Location of Attacked Switch	OOSL	Output of Proposed Algorithm	T _{est} (ms)	RL	EL ₁	EL ₂	EL ₃	EL ₄	EL ₅	EL ₆	EL ₇
41	j-q	SW ^C ₁₇	192	j-q	✓	✓	✓	✓	✓	✓	✓
42	k-q	SW ^C ₇₂	193	k-q	✓	✓	✓	✓	✓	✓	✓
43	l-q	SW ^C ₁₇	197	l-q	✓	✓	✓	✓	✓	✓	✓
44	o-q	SW ^C ₁₇	193	o-q	✓	✓	✓	✓	✓	✓	✓
45	p-q	SW ^C ₁₇	193	p-q	✓	✓	✓	✓	✓	✓	√
46	m-n	SW ^C ₇₂	197	m-n	✓	✓	✓	✓	✓	✓	√
47	n	SW ^C ₇₂	199	n	✓	✓	✓	✓	✓	✓	√
48	r-z	SW ^C ₂₁	197	r-z	✓	✓	✓	✓	✓	✓	✓
49	S-Z	SW ^C ₂₁	190	S-Z	✓	✓	✓	✓	✓	✓	√
50	t-z	SW ^C ₂₁	192	t-z	✓	✓	✓	✓	✓	✓	✓
51	u-z	SW ^C ₂₁	193	u-z	✓	✓	✓	✓	✓	✓	√
52	V-Z	SW ^C ₂₁	195	V-Z	✓	✓	✓	✓	✓	✓	√
53	W-Z	SW ^C ₂₁	195	W-Z	✓	✓	✓	✓	✓	✓	√
54	X-Z	SW ^C ₂₁	195	X-Z	✓	✓	✓	✓	✓	✓	√
55	y-z	SW ^C ₂₁	196	y-z	✓	✓	✓	√	✓	✓	✓
56	Z	SW ^C ₂₁	195	Z	✓	✓	✓	✓	✓	✓	✓
57	A'-O'	SW ^O ₆₃ SW ^C ₂₀ SW ^C ₇₂	199	A'-O'	√	√	√	✓	√	√	√
58	K'-O'	SW ^C ₇₂	198	K'-O'	✓	✓	✓	√	✓	✓	√
59	L'-O'	SW ^C ₇₂	199	L'-O'	✓	✓	✓	√	✓	✓	✓
60	M'-O'	SW ^C ₇₂	196	M'-O'	✓	✓	✓	✓	✓	✓	✓
61	N'-O'	SW ^C ₇₂	197	N'-O'	✓	✓	✓	√	✓	✓	✓
62	O'	SW ^C ₇₂	196	Ο′	✓	✓	✓	✓	✓	✓	✓
63	B'-I'	SW ^C ₂₀	198	B'-I'	✓	✓	✓	✓	✓	✓	√
64	C'-I'	SW ^C ₂₀	198	C'-I'	✓	✓	✓	✓	✓	✓	√
65	D'-I'	SW ^C ₂₀	199	D'-I'	✓	✓	✓	✓	✓	✓	√
66	E'-I'	SW ^C ₂₀	190	E'-I'	✓	✓	✓	✓	✓	✓	✓
67	F'-I'	SW_{20}^C	199	F'-I'	✓	✓	✓	✓	✓	✓	✓
68	G'-I'	SW ^C ₂₀	196	G'-I'	✓	✓	✓	✓	✓	✓	✓
69	H'-I'	SW_{20}^C	198	H'-I'	✓	✓	✓	✓	✓	✓	√
70	I'	SW ^C ₂₀	199	I'	✓	✓	✓	√	√	✓	√
71	q	SW ^C ₁₇	192	q	✓	√	√	√	√	✓	√

There are many infeasible solutions that the proposed algorithm does not generate. Among the infeasible solutions is SW_{17}^C , which breaks the EL related to the overloading of feeder F3, with the subsequent outage of its loads and without supply recovery of the OOSL from A through P. The second infeasible solution is SW_{19}^C , which breaks the EL related to the overloading of feeder F2, with a subsequent outage for its loads and without supply recovery of the OOSL from A through P. The third infeasible solution is SW_{20}^C , which

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breaks the EL related to the overloading of feeder F4, with a subsequent outage for its loads and without supply recovery of the OOSL from A through P. The fourth infeasible solution is SW_{13}^O , SW_8^O , SW_{17}^C , SW_{20}^C , SW_{18}^C , which leads to the breakage of the EL related to this sequence of ACSs. The fifth infeasible solution is SW_{13}^O , SW_7^O , SW_8^O , SW_{17}^C , SW_{20}^C , SW_{18}^C , SW_{19}^C , which breaks the EL related to minimizing the number of ACSs.

The proposed algorithm succeeds in recovering the OOSL in the SDS following exposure to a single CA for all 66 possible cases, with efficiency of 100%—see Table 2. The electric supply restoration time for each possible solution for a single CA lies within the range of 190–199 ms. The limit of the node voltage when applying the proposed algorithm following exposure to a single CA lies within the range of 0.98–0.99 pu—see Figure 6. The total system power loss after applying the proposed algorithm following exposure to a single CA lies within the range of 1.056–1.235%. Such power loss is much smaller than that in a classical 70-bus SDS with four electric supply feeders [32]—see Figure 7.

Table 2. Efficiency of the proposed algorithm in recovering the OOSL in the SDS following exposure to a single CA, as well as two, three, four, and five simultaneous CAs.

Number of Simultaneous CAs	1	2	3	4	5
Efficiency	100%	100%	97.6%	97.1%	96.4%

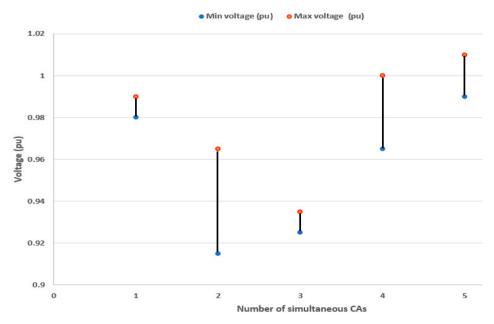


Figure 6. Voltage limits as predicted by the proposed algorithm following exposure to a single CA, as well as two, three, four, and five simultaneous CAs: for exposure to a single CA, the voltage lies within the range 0.98–0.99 pu; for exposure to two simultaneous CAs, it lies within the range 0.915–0.965 pu; for exposure to three simultaneous CAs, it lies within the range 0.925–0.935 pu; for exposure to four simultaneous CAs, it lies within the range 0.965–1.0 pu; and for exposure to five simultaneous CAs, it lies within the range 0.99–1.01 pu.

It is worth mentioning that the cyber-attack will not hit switches 17 through 21 as these represent tie switches in the system, which are usually open ones. If the CA hits the tie switch to be closed, the system automatically opens a sectionalized switch to maintain the radiality of the system without intervention with the proposed algorithm.

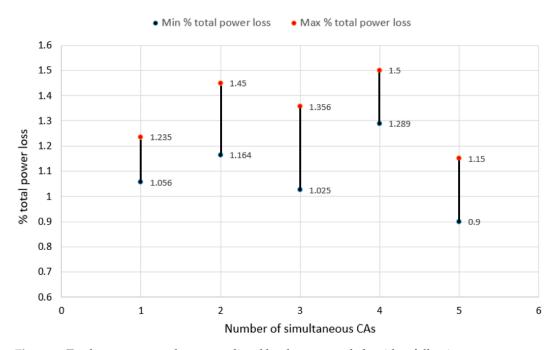


Figure 7. Total system power loss as predicted by the proposed algorithm following exposure to a single CA, as well as two, three, four, and five simultaneous CAs: for exposure to a single CA, it lies within the range 1.056–1.235%; for exposure to two simultaneous CAs, it lies within the range 1.164–1.45%; for exposure to three simultaneous CAs, it lies within the range 1.025–1.356% pu; for exposure to four simultaneous CAs, it lies within the range 1.289–1.5%; and for exposure to five simultaneous CAs, it lies within the range 0.9–1.15%.

3.2. Electric Service Recovery in SDS Following Exposure to Two Simultaneous CAs

For two simultaneous CAs, the number of possible cases is equal to 2145. Table 3 shows examples of the performance of the proposed algorithm when the SDS is exposed to two simultaneous CAs. The proposed algorithm achieves self-healing under all possible cases of exposure to two simultaneous CAs. The supply recovery time for each possible solution under two simultaneous CAs lies within the range of 190–199 ms. For two simultaneous CAs occurring at ACSs No. 1 and 32, the load nodes from A through P and from node a through node c are disconnected. The proposed algorithm generates a feasible output in the sequence SW_{13}^O , SW_{59}^O , SW_{52}^O , SW_{72}^C , SW_{17}^C , SW_{18}^C , SW_{21}^C , which results in the supply recovery of all OOSLs in 197 ms, without breaking the ELs.

Table 3. Performance of the proposed algorithm under samples of maneuvering processes following two simultaneous cyber-attacks hitting the investigated 70-bus test system with four electric supply feeders.

Locations of Attacked Switches	OOSL	Output of Proposed Algorithm	T _{res} (ms)	RL	EL_1	EL ₂	EL ₃	EL ₄	EL ₅	EL ₆	EL ₇
1, 32	A-P, a-c	SW ₁₃ SW ₅₉ SW ₅₉ SW ₅₂ SW ₂₀ SW ₇₂ SW ₁₇ SW ₁₈ SW ₂₁	197	A-P, a-c	√	√	√	√	√	√	√

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Table	е З.	Cont.

Locations of Attacked Switches	OOSL	Output of Proposed Algorithm	T _{res} (ms)	RL	EL_1	EL ₂	EL ₃	EL_4	EL ₅	EL ₆	EL ₇
52, 68	v-z, G'-I'	SW_{20}^{C} SW_{21}^{C}	196	v-z, G'-I'	✓	✓	✓	✓	✓	✓	✓
31, 13	Z, a-c, I-L	SW ^C ₁₈ SW ^C ₁₇	195	Z, a-c, I-L	✓	✓	✓	✓	✓	✓	√
44, 45	p-q	SW ^C ₁₇	196	p-q	✓	✓	✓	✓	✓	✓	√
35, 43	d-f, m-q	SW ^O ₄₄ SW ^C ₇₂ SW ^C ₁₉ SW ^C ₁₇	197	d-f, m-q	✓	✓	✓	✓	✓	✓	√

The proposed algorithm succeeds in recovering the OOSL in the SDS following exposure to two simultaneous CAs in all 2145 cases, with efficiency of 100%—see Table 2. Applying the proposed algorithm with exposure to two simultaneous CAs results in node voltages in the range of 0.915–0.965 pu—see Figure 6—and total system power losses within the range of 1.164–1.45%. Such power loss is much smaller than that in a classical 70-bus SDS with four electric supply feeders [32]—see Figure 7.

3.3. Electric Service Recovery in SDS Following Exposure to Three Simultaneous CAs

For three simultaneous CAs, the number of possible cases is equal to 45,760. Table 4 shows examples of the performance of the proposed algorithm when the SDS is exposed to three simultaneous CAs. The proposed algorithm achieves efficiency equal to 97.6% under all possible cases of exposure to three simultaneous CAs. The supply recovery time for each possible case of three simultaneous CAs lies in the range of 190–199 ms. For three simultaneous CAs occurring at ACSs No. 35, 54, and 44, the load nodes from d through f, from x through z, and from o through q are disconnected. The proposed algorithm generates a feasible output in the sequence SW_{19}^C , SW_{17}^C , SW_{21}^C , which results in the supply recovery of all OOSLs in 197 ms, without breaking the ELs.

The proposed algorithm succeeds in recovering the OOSL in the SDS following exposure to three simultaneous CAs in 44,662 cases among the total of 45,760, with efficiency of 97.6%—see Table 2. Applying the proposed algorithm with exposure to three simultaneous CAs results in node voltages in the range of 0.925–0.935 pu—see Figure 6—and total system power losses within the range of 1.025–1.356%, which is much smaller than that in a classical 70-bus SDS with four electric supply feeders [32]—see Figure 7.

Table 4. Performance of the proposed algorithm under samples of maneuvering processes following three simultaneous cyber-attacks hitting the investigated 70-bus test system with four electric supply feeders.

Locations of Attacked Switches	OOSL	Output of Proposed Algorithm	T _{res} (ms)	RL	EL ₁	EL_2	EL ₃	EL_4	EL_5	EL_6	EL ₇
35, 54, 44	d-f, x-z, o-q	SW ^C ₁₉ SW ^C ₁₇ SW ^C ₂₁	197	d-f, x-z, o-q	✓	✓	✓	✓	✓	✓	✓
50, 58, 8	t-z, K'-O', H-P	SW ^C ₂₁ SW ^C ₂₂ SW ^C ₂₀	199	t-z, K'-O', H-P	√	✓	✓	✓	√	✓	√

Table 4. Cont.

Locations of Attacked Switches	OOSL	Output of Proposed Algorithm	T _{res} (ms)	RL	EL ₁	EL_2	EL ₃	EL_4	EL ₅	EL ₆	EL ₇
28, 1, 32	W-Y, A-P, a-c	SW ₁₃ SW ₅₉ SW ₅₀ SW ₅₂ SW ₂₀ SW ₇₂ SW ₁₇ SW ₁₈ SW ₂₁	197	W-Y, A-P, a-c	✓	√	✓	✓	✓	✓	√
46, 36, 34	m-n, e-f, c	SW ₇₂ SW ₁₉ SW ₁₈	190	m-n, e-f, c	√	✓	√	√	√	✓	√
15, 50, 58	K-L, t-z, K'-O'	SW ^C ₁₇ SW ^C ₂₁ SW ^C ₇₂	192	K-L, t-z, K'-O'	✓	✓	✓	✓	✓	√	√

3.4. Electric Service Recovery in SDS Following Exposure to Four Simultaneous CAs

For four simultaneous CAs, the number of possible cases is equal to 720,720. Table 5 shows examples of the performance of the proposed algorithm when the SDS is exposed to four simultaneous CAs. The proposed algorithm achieves efficiency equal to 97.1% under all possible cases of exposure to four simultaneous CAs. The supply recovery time for each possible case of four simultaneous CAs lies the range 190–199 ms. For four simultaneous CAs occurring at ACSs No. 9, 11, 45, and 54, the load nodes from M through O, from p through q, and from x through z are disconnected. The proposed algorithm generates a feasible output in the sequence SW_{18}^C , SW_{17}^C , SW_{21}^C , SW_{19}^C , which results in the supply recovery of all OOSLs in 190 ms, without breaking the ELs.

Table 5. Performance of the proposed algorithm under samples of maneuvering processes following four simultaneous cyber-attacks hitting the investigated 70-bus test system with four electric supply feeders.

Locations of Attacked Switches	OOSL	Output of Proposed Algorithm	T _{res} (ms)	RL	EL ₁	EL ₂	EL ₃	EL ₄	EL ₅	EL ₆	EL ₇
9, 11, 45, 54	M-O, p-q, x-z	SW_{18}^{C} SW_{17}^{C} SW_{21}^{C} SW_{19}^{C}	190	M-O, p-q, x-z	✓	✓	✓	√	✓	√	√
62, 28, 1, 9	O, W-Y, A-P, a-c	SW ₁₃ SW ₁₉ SW ₁₉ SW ₅₉ SW ₅₂ SW ₂₀ SW ₇₂ SW ₇₂ SW ₁₇ SW ₁₈ SW ₂₁	197	O, W-Y, A-P, a-c	4	√	√	√	✓	√	√

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Table 5. Cont.

Locations of Attacked Switches	OOSL	Output of Proposed Algorithm	T _{res} (ms)	RL	EL ₁	EL_2	EL ₃	EL_4	EL_5	EL ₆	EL ₇
29, 70, 44, 11	x-y, I'-I', o-q, M-N	SW ^C ₂₁ SW ^C ₂₀ SW ^C ₁₇ SW ^C ₁₈	196	x-y, I'-I', o-q, M-N	✓	√	√	√	✓	✓	√
71, 14, 8, 12	I', J-L, H, O-P, N	SW_{19}^{C} SW_{17}^{C} SW_{20}^{C} SW_{18}^{C}	193	I', J-L, H, O-P, N	✓	✓	✓	✓	✓	✓	√
60, 52, 5, 72	M'-O', v-z, E-H, M-P, q	SW ^C ₂₁ SW ^C ₇₂ SW ^C ₁₉ SW ^C ₁₇	193	M'-O', v-z, E-H, M-P, q	✓	✓	✓	✓	✓	✓	✓

The proposed algorithm succeeds in recovering the OOSL in the SDS following exposure to four simultaneous CAs in 699,819 cases among the total of 720,720, with efficiency of 97.1%—see Table 2. The limit of the node voltage after applying the proposed algorithm under exposure to four simultaneous CAs lies within the range of 0.965–1.0 pu—see Figure 6—with a range of 1.289-1.5% for the total system power loss. Such power loss is much smaller than that in a classical 70-bus SDS with four electric supply feeders [32]—see Figure 7.

3.5. Electric Service Recovery in SDS Following Exposure to Five Simultaneous CAs

For five simultaneous CAs, the number of possible cases is equal to 8,936,928. Table 6 shows examples of the performance of the proposed algorithm when the SDS is exposed to five simultaneous CAs. The proposed algorithm achieves efficiency equal to 96.4% under all possible cases of exposure to five simultaneous CAs. The supply recovery time for each possible case of five simultaneous CAs lies in the range 190–199 ms. For five simultaneous CAs occurring at ACSs No. 32, 28, 62, 44, and 11, the load nodes from W through Y, from o through q, from M through N, and f and N are disconnected. The proposed algorithm generates a feasible output in the sequence SW_{21}^C , SW_{72}^C , SW_{19}^C , SW_{17}^C , SW_{18}^C , which results in the supply recovery of all OOSLs in 199 ms, without breaking the ELs.

Table 6. Performance of the proposed algorithm under samples of maneuvering processes following five simultaneous cyber-attacks hitting the investigated 70-bus test system with four electric supply feeders.

Locations of Attacked Switches	OOSL	Output of Proposed Algorithm	T _{res} (ms)	RL	EL ₁	EL_2	EL ₃	EL_4	EL ₅	EL ₆	EL ₇
37, 28, 62, 44, 11	f, W-Y, O', o-q, M-N	SW ₂₁ SW ₇₂ SW ₇₂ SW ₁₉ SW ₁₇ SW ₁₈	199	f, W-Y, O', o-q, M-N	✓	✓	√	✓	✓	✓	√

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Table 6. Cont.

Locations of Attacked Switches	OOSL	Output of Proposed Algorithm	T _{res} (ms)	RL	EL ₁	EL ₂	EL ₃	EL ₄	EL ₅	EL ₆	EL ₇
15, 55, 8, 69, 46	K-L, y-z, H, O-P, H'-I', m-n	SW_{17}^{C} SW_{19}^{C} SW_{21}^{C} SW_{20}^{C} SW_{72}^{C}	199	K-L, y-z, H, O-P, H'-I', m-n	√	√	√	✓	✓	✓	✓
45, 47, 56, 9	O, p-q, n, z	SW ^C ₂₀ SW ^C ₇₂ SW ^C ₁₇ SW ^C ₁₉ SW ^C ₂₁	193	O, p-q, n, z	✓	√	√	✓	✓	√	√
53, 47, 10, 36, 16	w-z, n, P, e-f, L	SW_{21}^{C} SW_{72}^{C} SW_{20}^{C} SW_{19}^{C} SW_{17}^{C}	196	w-z, n, P, e-f, L	√	√	√	✓	✓	√	✓
14, 68, 50, 11, 61	J-L, G'-I', t-z, M-N, N'-O'	SW_{20}^{C} SW_{21}^{C} SW_{17}^{C} SW_{18}^{C} SW_{72}^{C}	194	J-L, G'-I', t-z, M-N, N'-O'	✓	✓	✓	✓	✓	✓	✓

The proposed algorithm succeeds in recovering the OOSL in the SDS following exposure to five simultaneous CAs in 8,615,199 cases among the total of 8,936,928, with efficiency of 96.4%—see Table 2. The limit of the node voltage after applying the proposed algorithm under exposure to five simultaneous CAs lies within the range 0.99–1.01 pu—see Figure 6—with a range of 0.9-1.15% for the total system power loss. Such power loss is much smaller than that in a classical 70-bus SDS with four electric supply feeders [32]—see Figure 7. Table 2 summarizes the efficiency of the proposed algorithm in recovering the OOSL in the SDS following exposure to a single and simultaneous CAs.

Table 7 shows a comparison between the proposed algorithm and other algorithms reported in the literature.

Table 7. A comparison between the proposed algorithm and other algorithms reported in the literature.

Reference	Contribution	Advantages	Disadvantages	
[27]	The study aimed to recover the out-of-service zones in the smart grid after experiencing a CA by ensuring the system's recovery from the threat and removing the attack itself in a 39-bus and IEEE 30-bus setup.	Enhanced the reliability and resilience by 22%.	The authors did not take the electric limitations into consideration.	
[28]	The authors increased the number of personnel after a CA to recover the EC for the OOSL.	The algorithm succeeds in guaranteeing the continuity of the supply after a single CA.	The restoration time is high due to reliance on human intervention.	

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Table 7. Cont.

Reference	Contribution	Advantages	Disadvantages	
[29]	The algorithm's contribution is based on enhancing the ability of an SDS to withstand a CA by using large number of electric vehicles as distributed generators to feed the OOSL after a CA.	The number of recovered OOSLs is increased with the help of electric vehicles and DGs.	Dependence on high penetration level of distributed generators.	
[30]	The authors sought to recover a part of the outage area under a CA by adding DG resources to support the smart distribution system against CAs.	The algorithm showed better performance regarding the reliability indices.	Low performance in simultaneous CAs.	
[31]	The authors proposed an optimized algorithm based on mixed-integer linear programming to address load interruptions following a CA. The algorithm was based on the philosophy of first fail first repair.	The results of the algorithm showed better performance as regards the number of recovered out-of-service loads.	Violation of the electrical limitation related to load priority.	
Proposed algorithm	A novel algorithm is proposed for the first time to recover the ES to the OOSL after a CA on an ACS in the SDS, regardless of whether the CA occurs on a single ACS or multiple ACSs.	The proposed algorithm showed better performance according to (a) the time of electric service recovery, (b) achieving self-healing, (c) testing under single and simultaneous CAs. The proposed algorithm showed better performance irrespective of (a) the number of recovered OOSLs, (b) the system size, (c) operation with or without DGs.	The efficiency decreases when the number of simultaneous CAs increases.	

4. Conclusions

An algorithm is proposed to recover the electric supply for OOSLs in the SDS after exposure to a CA resulting in interruptions in the INSL. The proposed algorithm is based on three steps. The first step is based on building the SDS in matrix form. The second step is based on classifying the SDS into three zones: the attacked zone and the primary and secondary neighbor zones. The third step is based on obtaining five types of MP to recover the OOSL without breaking the ELs.

The proposed algorithm takes into consideration the ELs related to the maximum branch current, the nodes' voltage, the load priority, the radiality maintenance of the SDS, the minimum total system power loss, and the instruction sequence of ACSs.

The proposed algorithm achieved self-healing after exposure to a single or double CAs without breaking the ELs when tested under a 70-bus SDS with four electric supply feeders.

The proposed algorithm succeeded in recovering the OOSLs in the investigated 70-bus SDS following exposure to a single CA in all 66 possible case studies, as well as in 2145 cases of exposure to two simultaneous CAs.

The proposed algorithm succeeded in recovering the OOSLs in the investigated 70-bus SDS following exposure to three simultaneous CAs in 44,662 cases out of 45,760, as well as in 699,819 cases out of 720,720 and 8,615,199 cases out of 8,936,928 of exposure to four and five simultaneous CAs, respectively.

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> The proposed algorithm achieved the recovery of the electric supply for three, four, and five ACSs exposed to CAs at efficiency values of 97.6%, 97.1%, and 96.4%, respectively, without breaking the ELs in the investigated 70-bus SDS.

> The mathematical model, computational requirements, and integration of the proposed algorithm with the hardware components represent a research gap for future work. Implementing a defense algorithm against cyber-threats is also a task for future work.

> In future research, the application of virtual bids [33] and mobile energy storage [34] in this context is also worth investigating.

> Recommendations for future researchers include the integration of modern technology like artificial intelligence, machine learning, big data, and data mining within this research topic.

> Challenges regarding merging the restoration algorithm with distribution power systems that contain hybrid switches, i.e., "manual and automatic" switches, should also be taken into consideration.

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Nomenclatures

$S_{(x,O)}$	Switch with name x and with status open
$S_{(y,C)}$	Switch with name y and with status closed
SW_x^C	Switch with name x and with status closed
SW_y^O	Switch with name y and with status open
ES	Electric service
OOSL	Out-of-service load
CA	Cyber-attack
ACS	Automatic communication switch
SDS	Smart distribution system
EL	Electric limitation
NO	Normally open
NC	Normally closed
INSL	In-service load
DG	Distributed generation
MP	Maneuvering process
RL	Recovered load
SCADA	Supervisory control and data acquisition
OT	Operational technology
IT	Information technology
IoT	Internet of Things

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